

COMPAS_sCO₂



Chromium-Silicon Alloys with Fe and Ni for Structural High Temperature Applications

M. Kerbstadt, E. White, A. S. Ulrich, M. C. Galetz



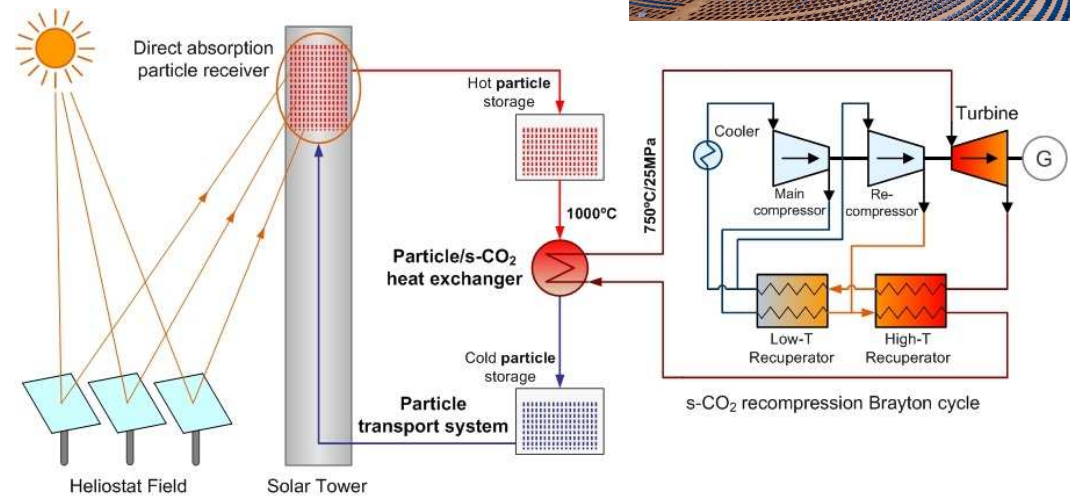
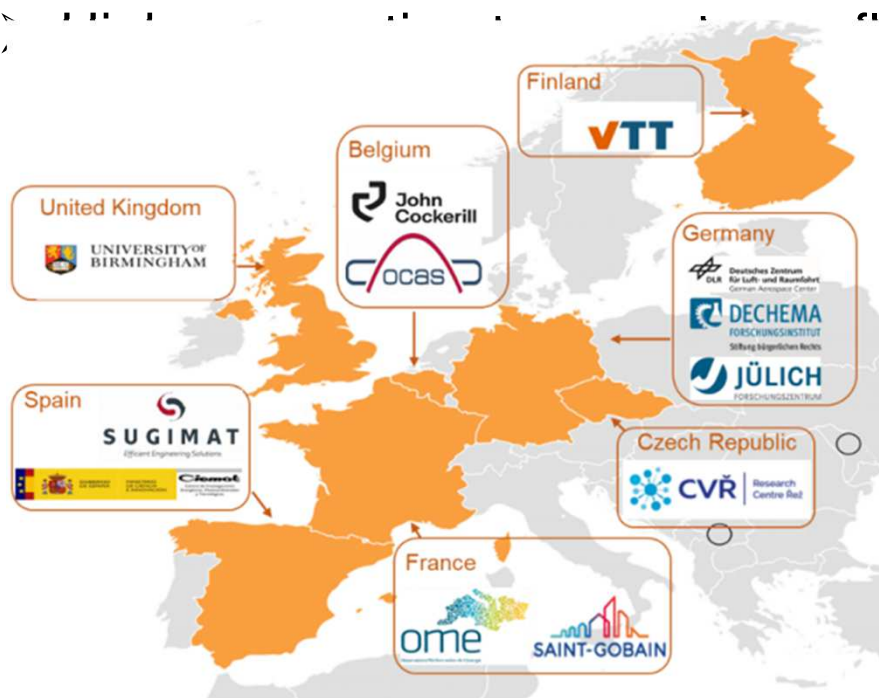
THIS PROJECT IS BEING FUNDED BY THE EUROPEAN UNION'S HORIZON 2020 RESEARCH AND INNOVATION PROGRAMME UNDER GRANT AGREEMENT NO 958418 COMPAS_sCO₂

CompassCO2: Next Gen. Concentrated Solar Plants

- Difference to state-of-the-art: ceramic particles for heat storage and s-CO₂ as working medium in Brayton Cycle

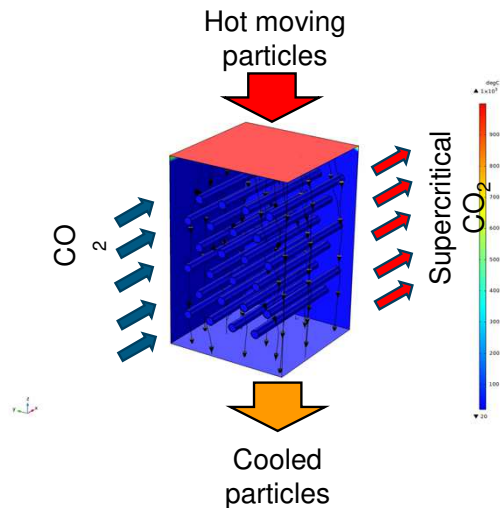


“exible day and night use



CompassCO2: Heat Exchanger

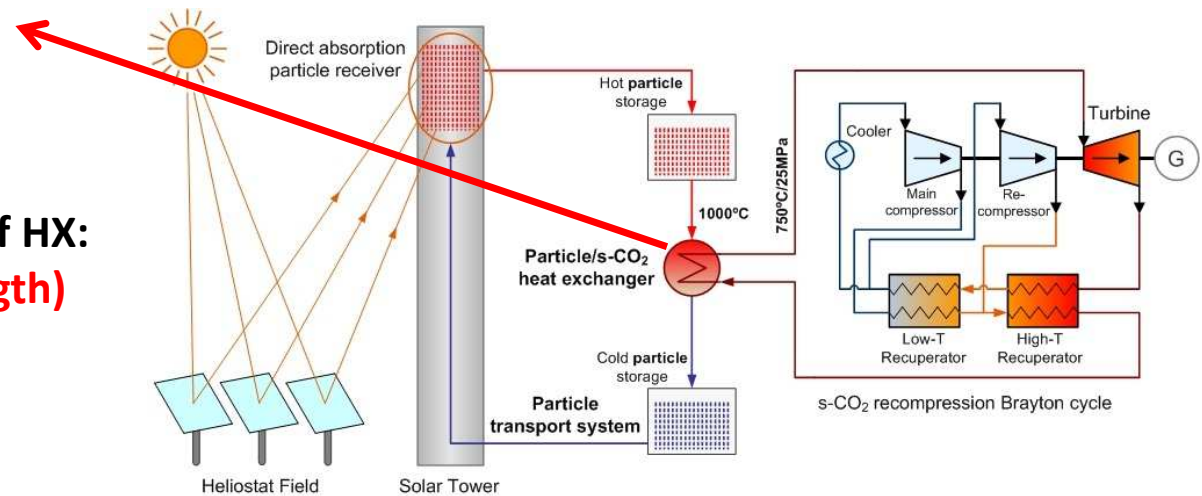
Heat exchanger (HX)



Challenges of structural materials of HX:

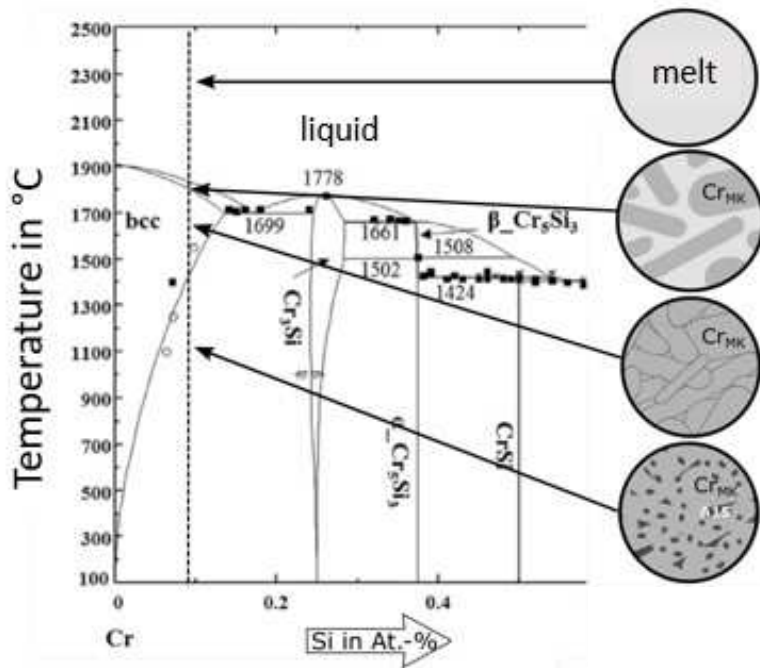
- High temperature >700°C (strength)
- s-CO₂ environment (corrosion)
- Erosion due to particles (wear)
- High pressure ~20 MPa

=> Cr-based materials

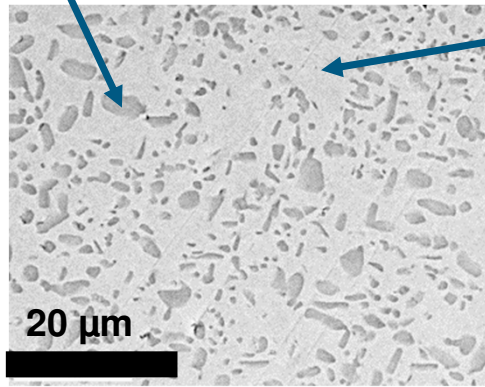


[www.compassco2.eu]

Candidate alloys: Heat Treatable Cr-Si Alloys

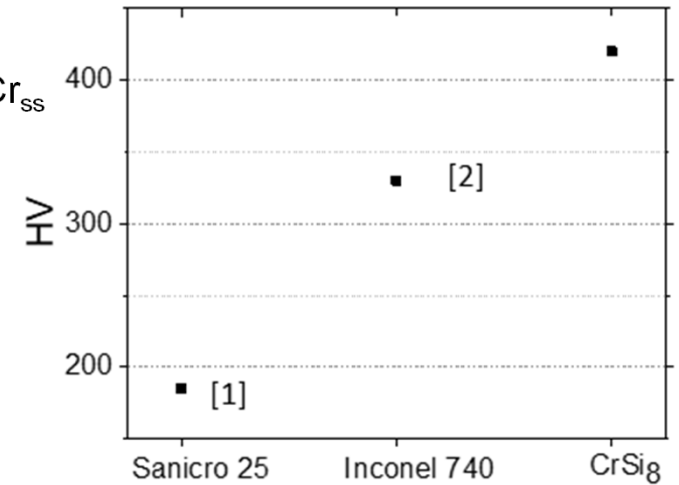


A15 Cr₃Si



Two-phase microstructure: Cr_{ss} + A15 Cr₃Si

Cr_{ss}

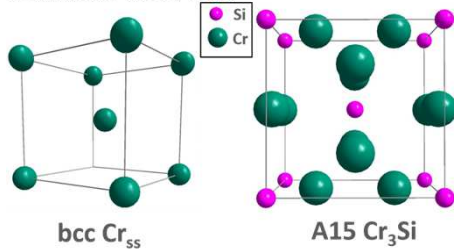


HV of Cr₉₀Si₈ compared to conventional materials*

[1] <https://www.materials.sandvik.com>, January 2022

[2] <https://www.azom.com>, January 2022

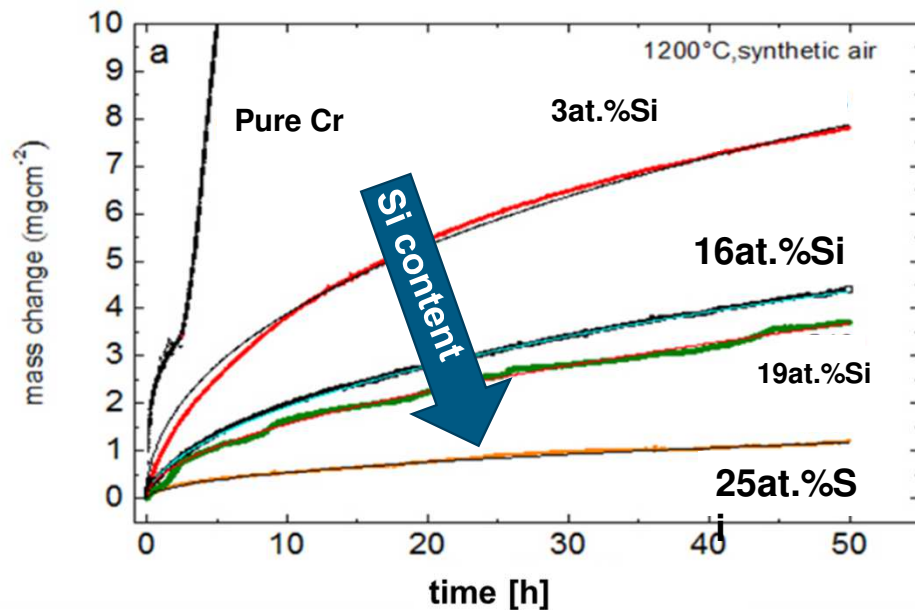
[A. S. Ulrich, PhD Thesis, 2020]



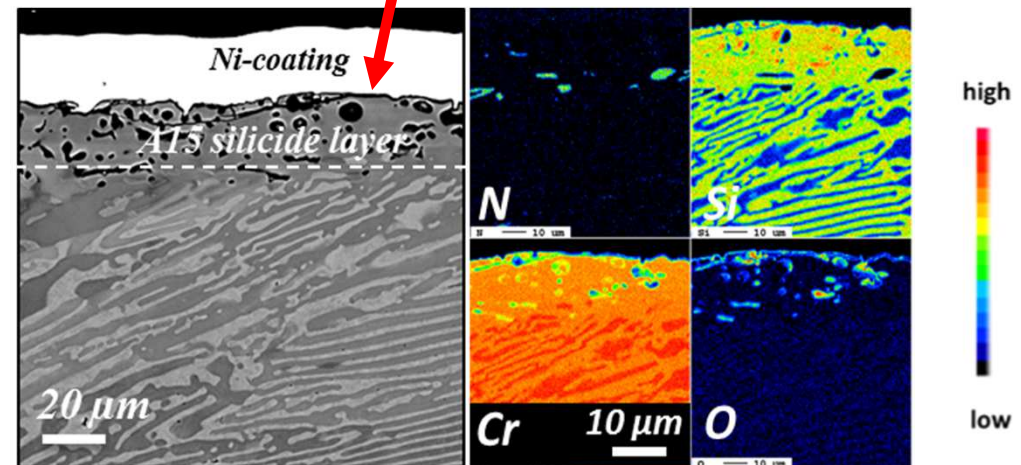
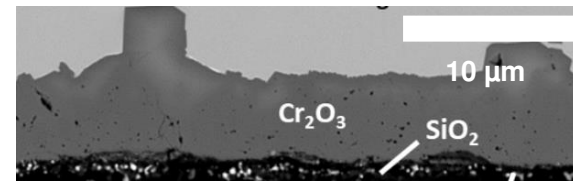
- 100 h @ 1200°C: Diffusion controlled precipitation of Cr₃Si-phase

Cr-Si Alloys: Advantages

50h @ 1200°C, air



Si decreases oxidation rate but also ductility



$\text{Cr}_{84}\text{Si}_{16}$: Layered oxid scale + continuous A15 Cr_3Si layer acts as a barrier to nitration

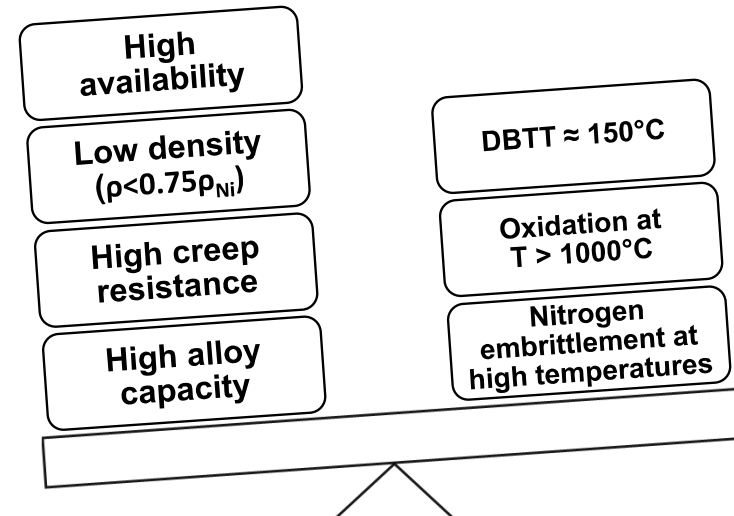
- Increasing amount of Si: improved oxidation and nitration resistance

A. Soleimani Dorcheh, W. Donner, M. C. Galetz, *Materials and Corrosion*, 2014

Cr-Based Alloys: Potentials and Challenges

Possibilities

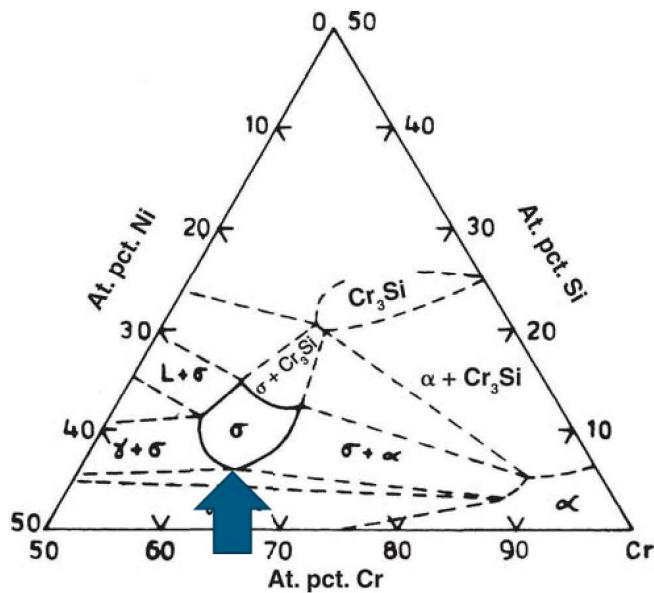
Challenges



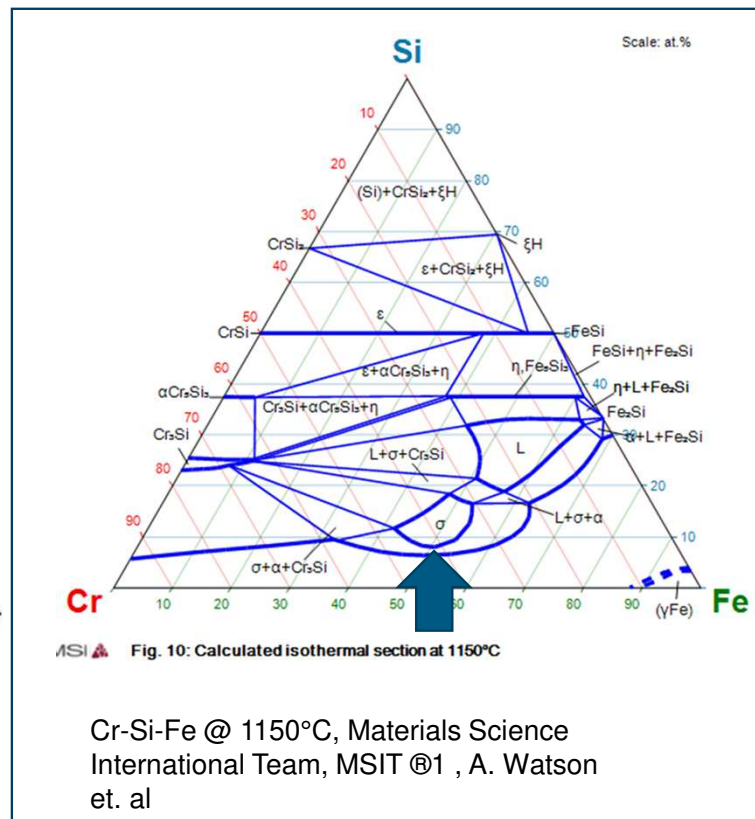
A. Soleimani Dorcheh, W. Donner, M. C. Galetz, Materials and Corrosion, 2014

Alloying with Iron and Nickel

Sigma-formers (might) have a ductilizing effect? **Rhenium effect**



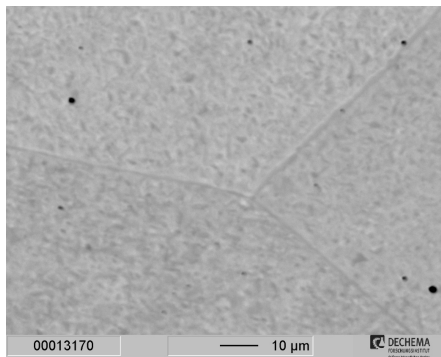
Cr-Si-Ni @ 1175°C, K.P. Gupta, Journal of Phase Equilibria and Diffusion Vol. 27 No. 5 2006



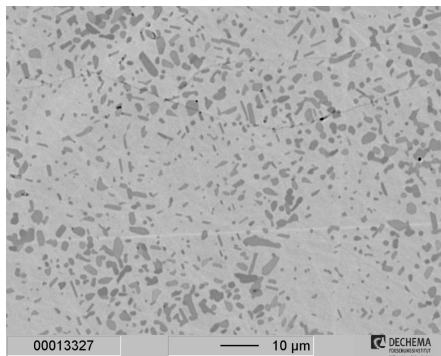
Cr-Si-Fe @ 1150°C, Materials Science International Team, MSIT @1, A. Watson et. al

- *Klopp W.D., Review of Ductilizing of Group VIA Elements by Rhenium and Other Solutes. National Aeronautics and Space Administration, 1968 [1]
- *Gilbert A., Allen B.C., Reid C.N., An investigation of mechanical properties of chromium, chromium-rhenium, and derived alloys; NASA CR-118, (1964) [2]
- *Stephens J.R.; Klopp W.D., Ductility Mechanisms and Superplasticity in Chromium Alloys. National Aeronautics [3]

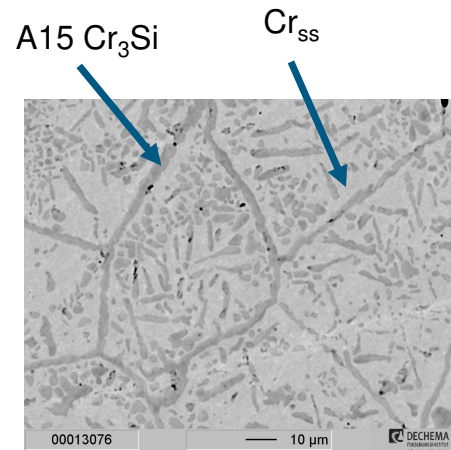
Alloying: Fe



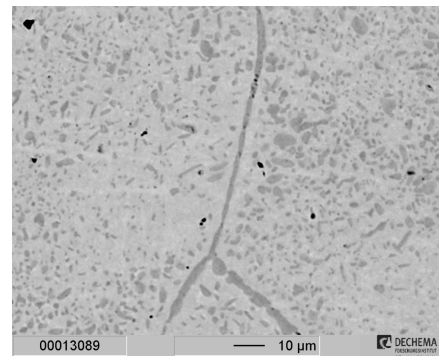
$\text{Cr}_{92}\text{Si}_8$



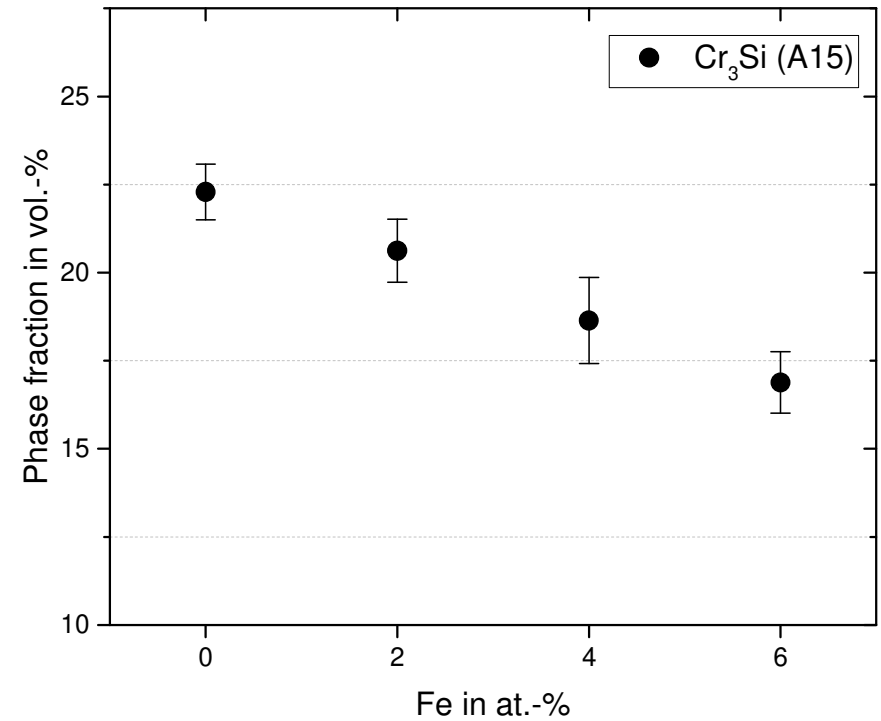
$\text{Cr}_{88}\text{Si}_8\text{Fe}_4$



$\text{Cr}_{90}\text{Si}_8\text{Fe}_2$



$\text{Cr}_{86}\text{Si}_8\text{Fe}_6$

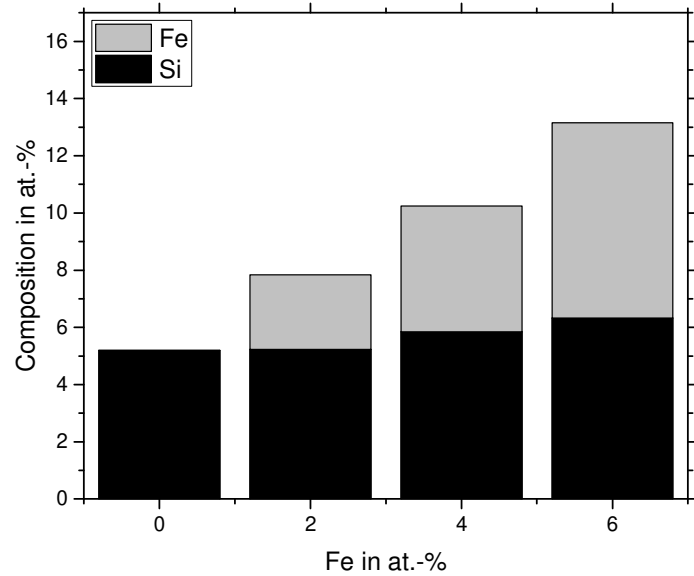


Cr_3Si fraction with of Fe amount

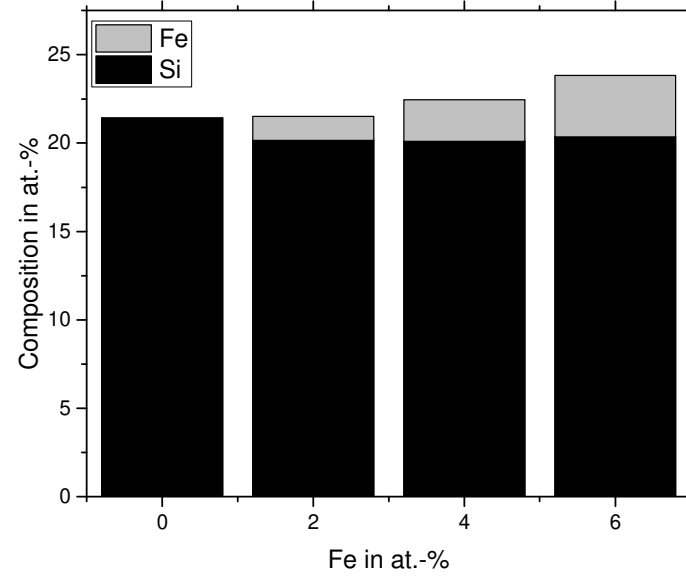
- Formation of desired two-phase microstructure
- Decreasing fraction of A15-precipitates with increasing amount of Fe

Cr-Si-Fe

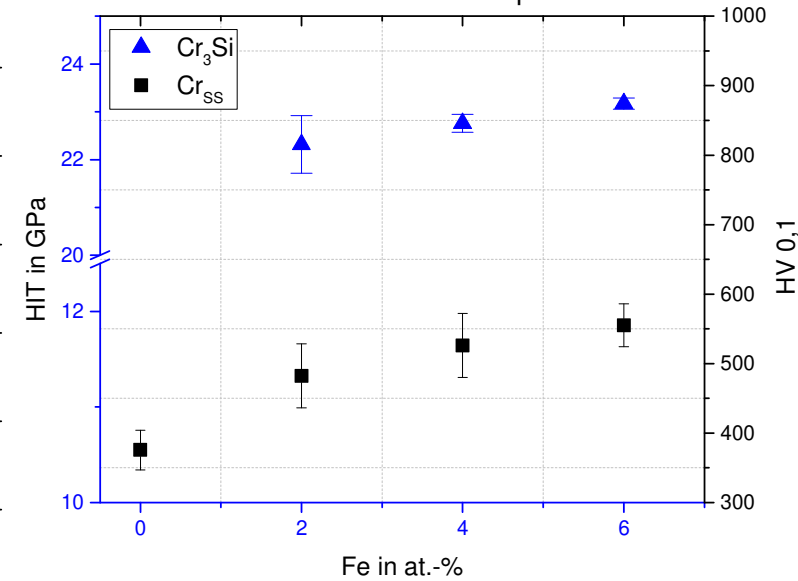
Composition of Cr_{SS}



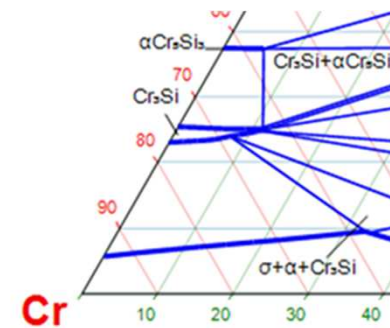
Composition of Cr₃Si



Nanohardness of different phases



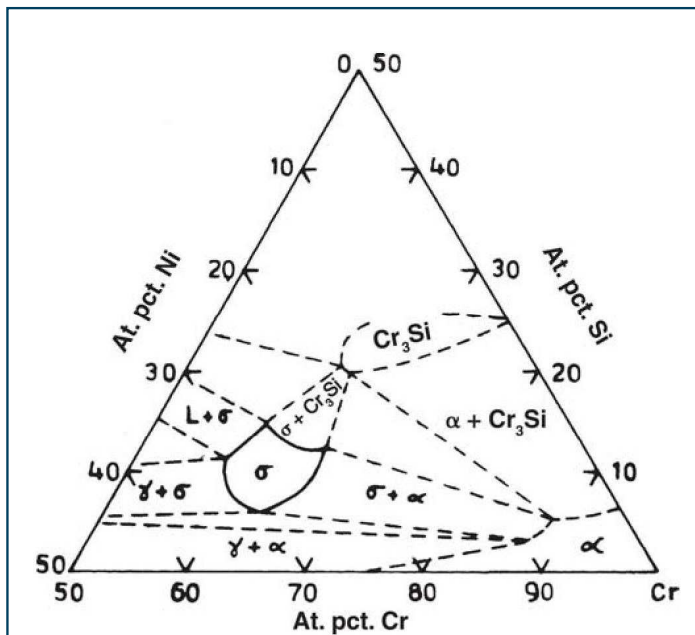
- Fe substitutes Cr in both phases, solubility of Si in Cr_{SS} increases with Fe, decreases in A15)
- **Hardness of both phases increases**



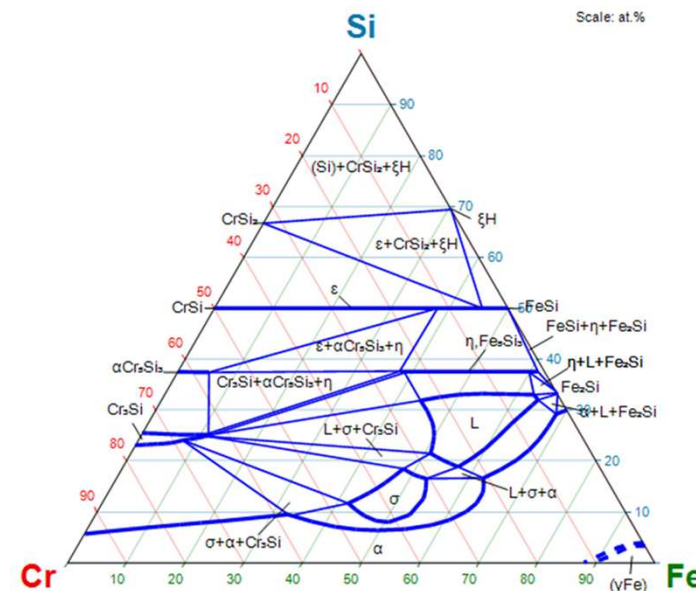
Alloying with Iron and Nickel

Fe and Ni

→ Systems interesting for development of Cr/Si diffusion coatings on Fe-/Ni-based substrates



Cr-Si-Ni @ 1175°C, K.P. Gupta, Journal of Phase Equilibria and Diffusion Vol. 27 No. 5 2006



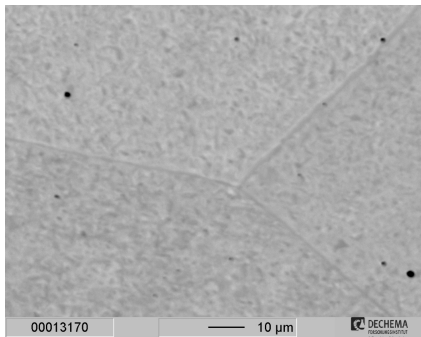
ASI Fig. 10: Calculated isothermal section at 1150°C

Cr-Si-Fe @ 1150°C, Materials Science International Team, MSIT @1, A. Watson et. al

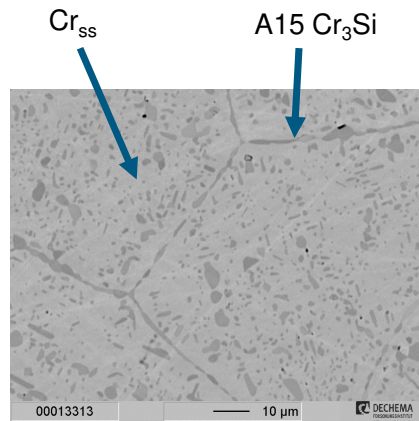
Sigma-formers might have a ductilizing effect (Rhenium effect)

- *Klopp W.D., Review of Ductilizing of Group VIA Elements by Rhenium and Other Solutes. National Aeronautics and Space Administration, 1968 [1]
- *Gilbert A., Allen B.C., Reid C.N., An investigation of mechanical properties of chromium, chromium-rhenium, and derived alloys; NASA CR-118, (1964) [2]
- *Stephens J.R.; Klopp W.D., Ductility Mechanisms and Superplasticity in Chromium Alloys. National Aeronautics [3]

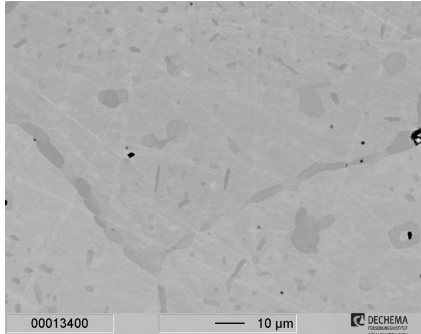
Alloying Ni



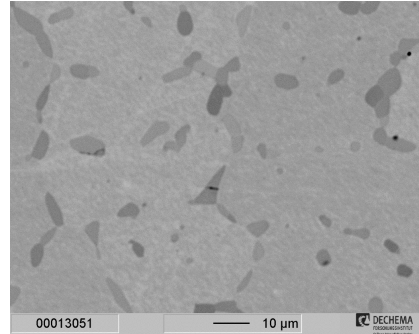
$\text{Cr}_{92}\text{Si}_8$



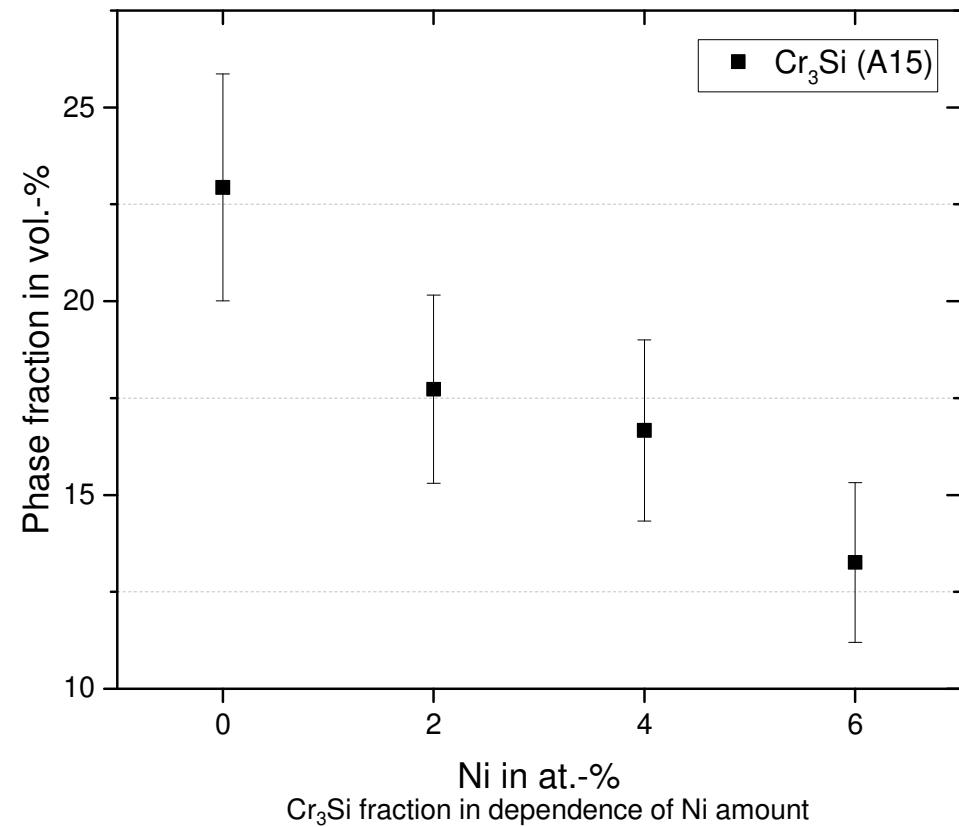
$\text{Cr}_{90}\text{Si}_8\text{Ni}_2$



$\text{Cr}_{88}\text{Si}_8\text{Ni}_4$



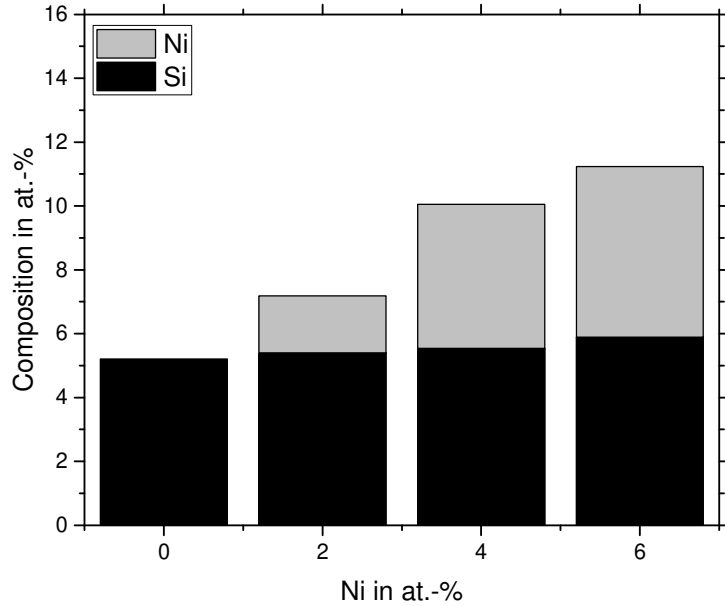
$\text{Cr}_{86}\text{Si}_8\text{Ni}_6$



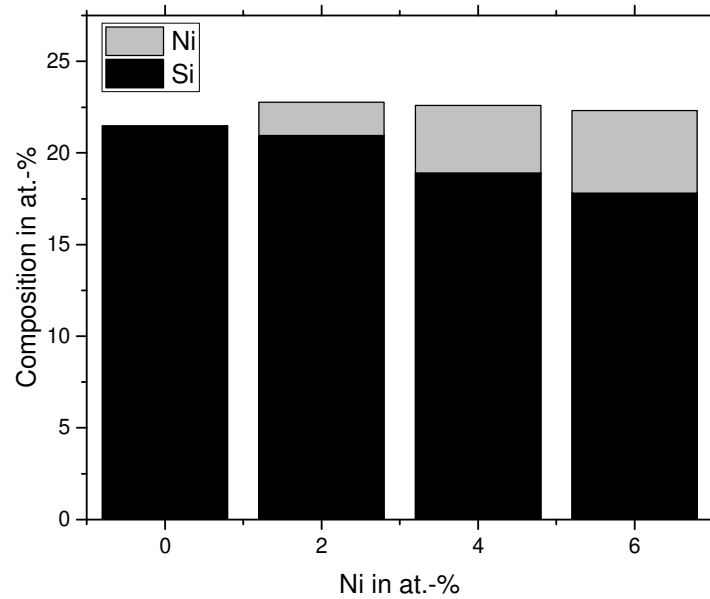
- Formation of the desired two-phase microstructure
- Decreasing fraction of A15 with increased amount of Ni

Cr-Si-Ni: Phase Analysis

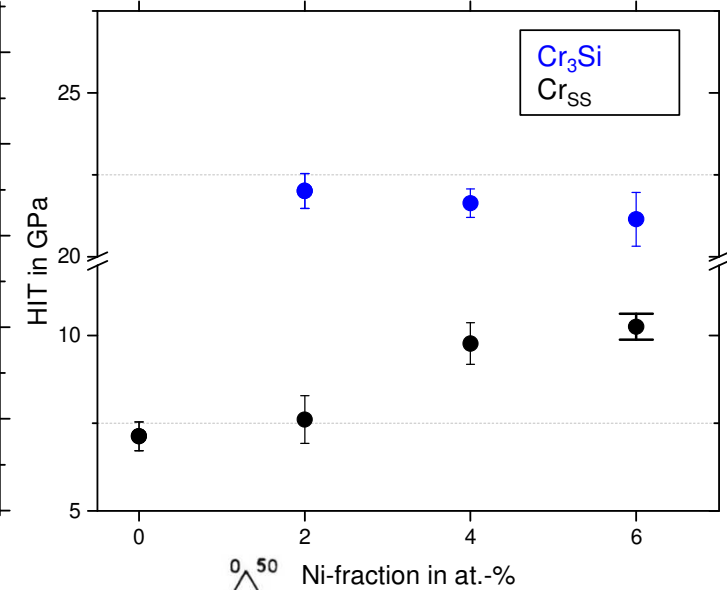
Composition of Cr_{SS}



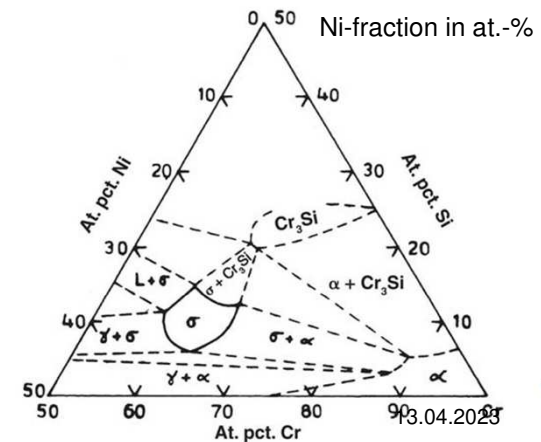
Composition of Cr₃Si



Nanohardness of different phases

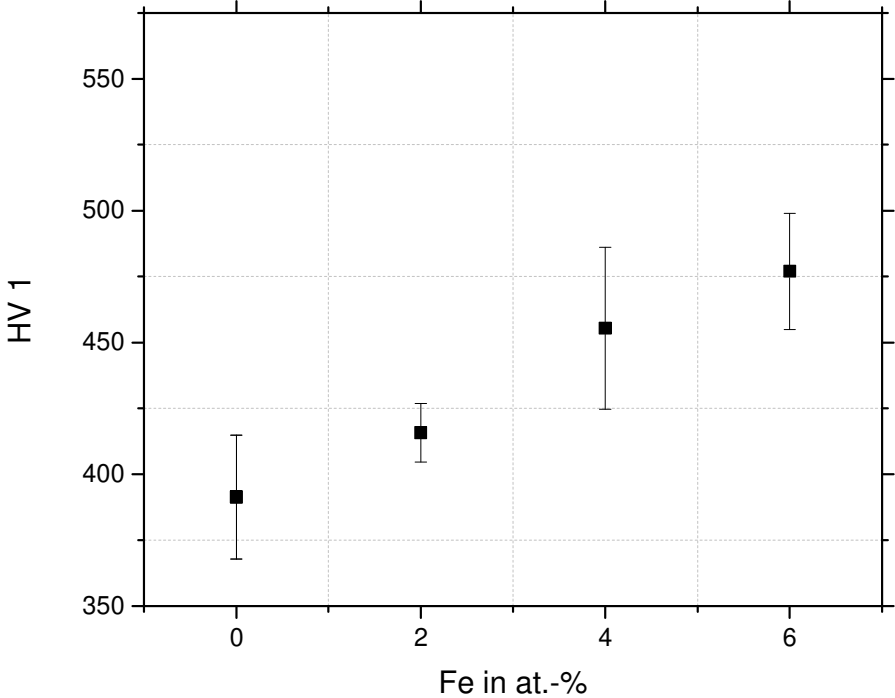


- Ni changes stichometry in Cr₃Si (Ni might substitute Si and Cr)
- **Hardness of Cr₃Si decreases with Ni and of Cr_{SS} increases**



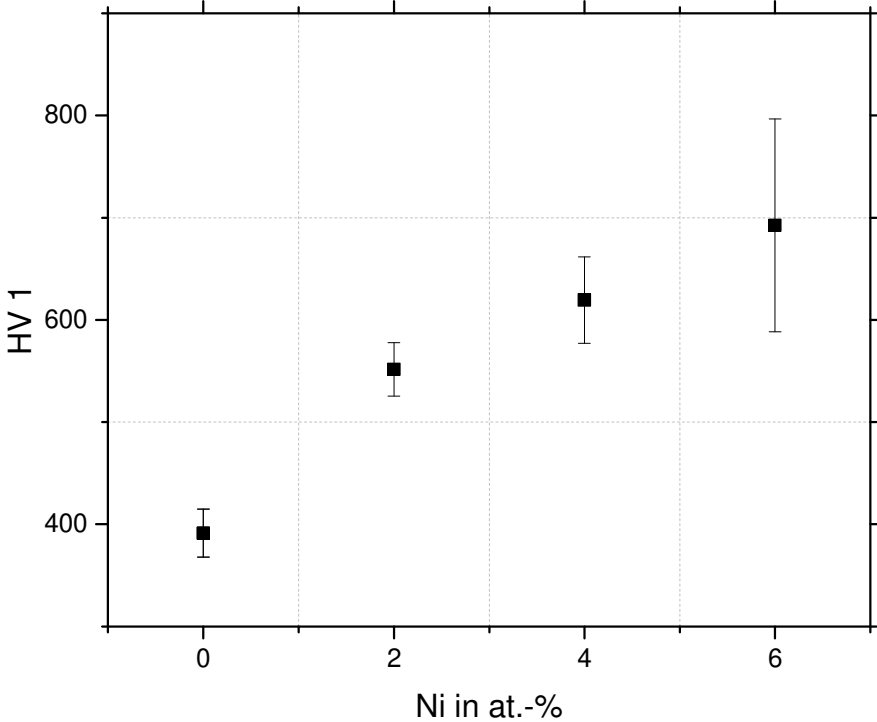
Microhardness

Cr-Fe-Si



➤ Microhardness increased by 28%

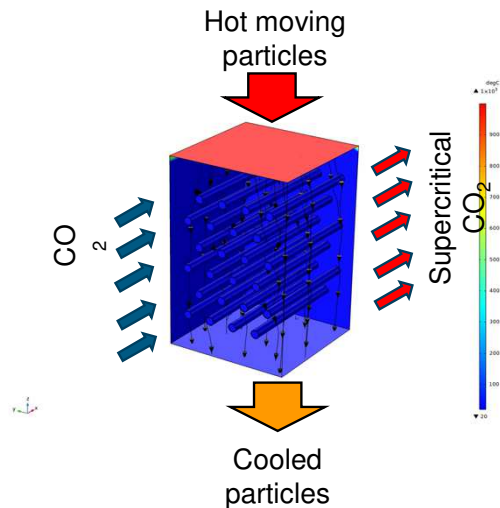
Cr-Si-Ni



➤ Microhardness increased by 75%
-> Ni much stronger Cr(ss)-hardener

CompassCO2: Heat Exchanger

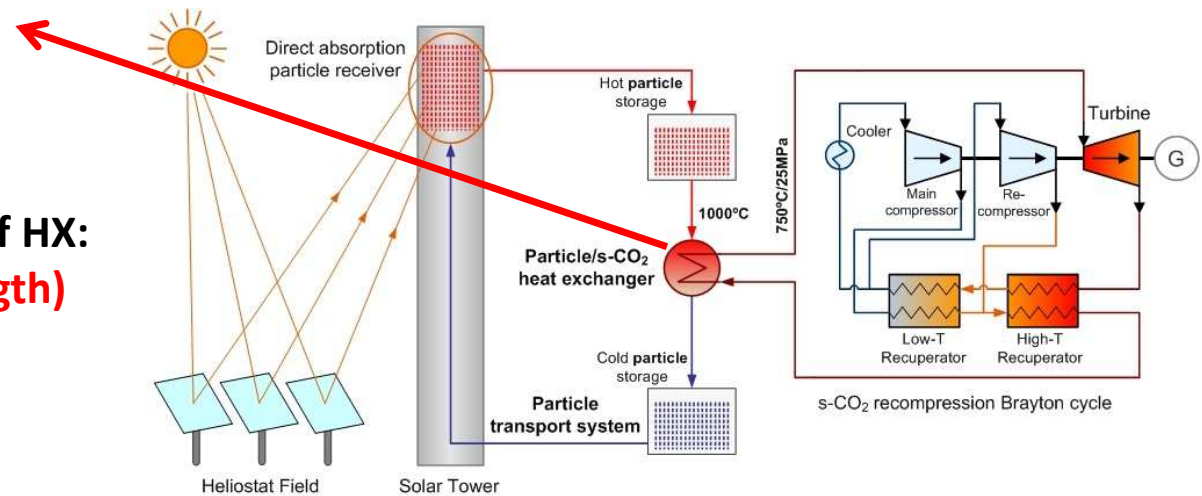
Heat exchanger (HX)



Challenges of structural materials of HX:

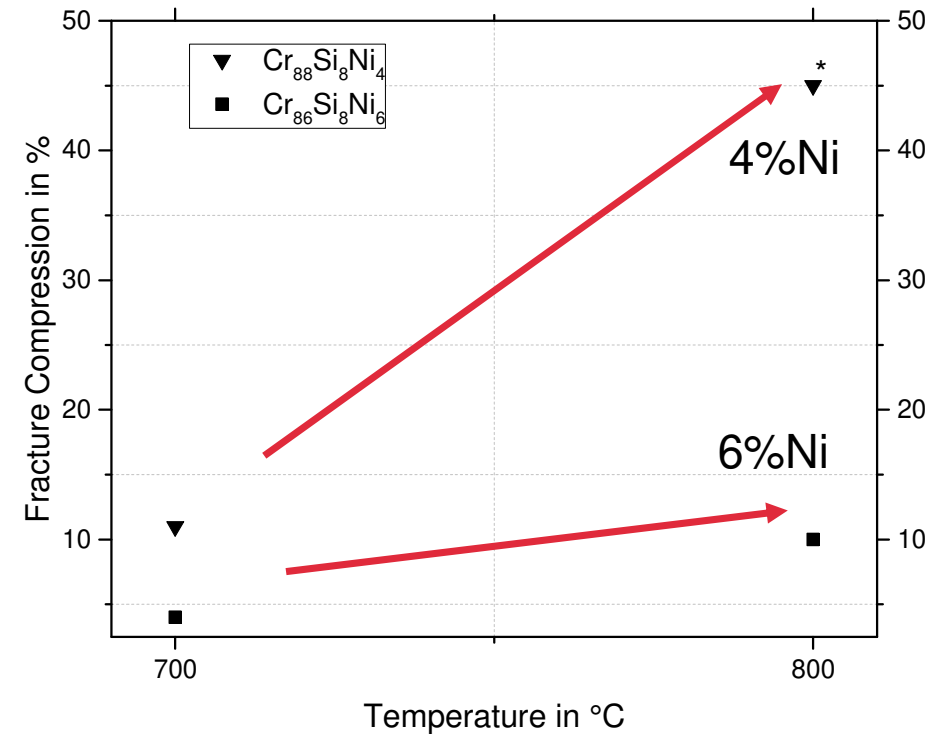
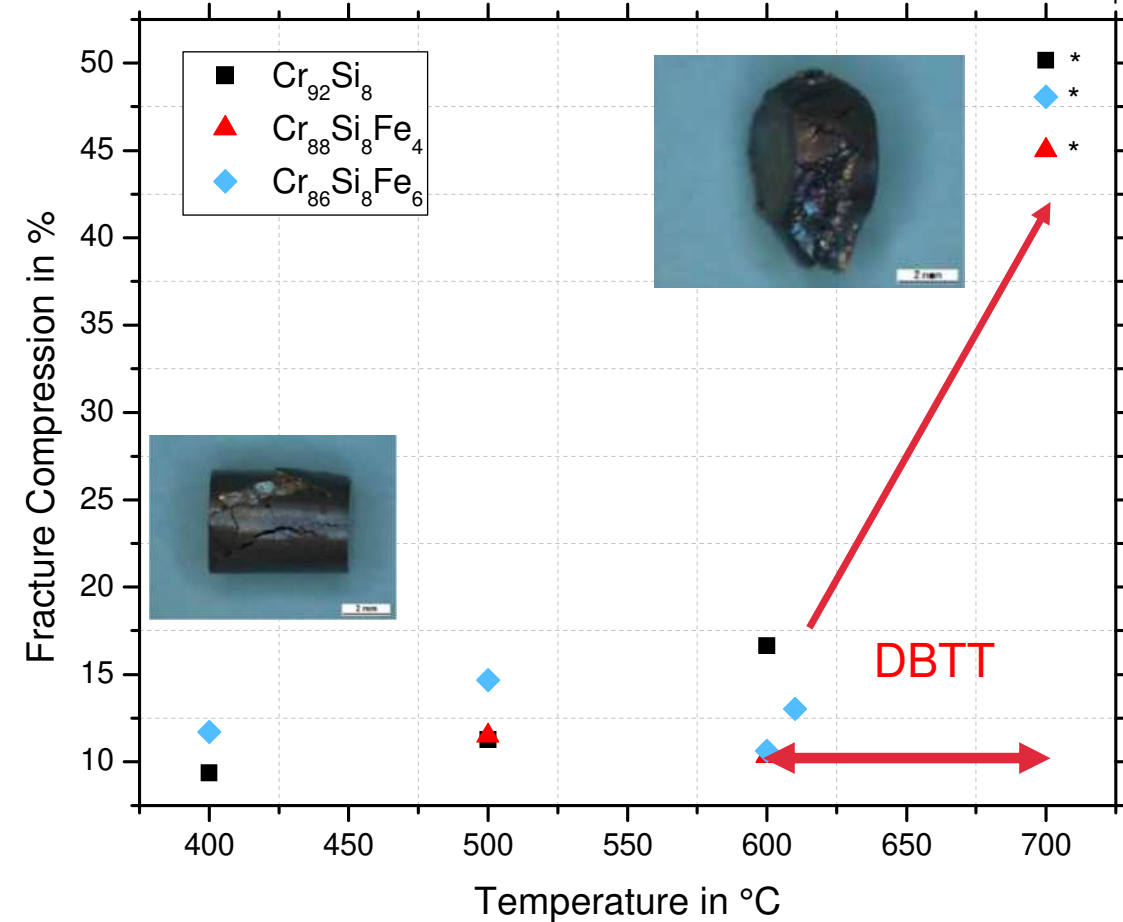
- High temperature >700°C (strength)
- s-CO₂ environment (corrosion)
- Erosion due to particles (wear)
- High pressure ~20 MPa

=> Cr-based materials



Cr-Si-Fe: DBTT by Compression Tests

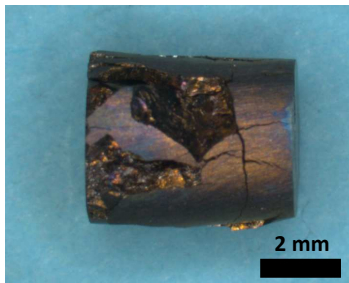
*samples did not fracture



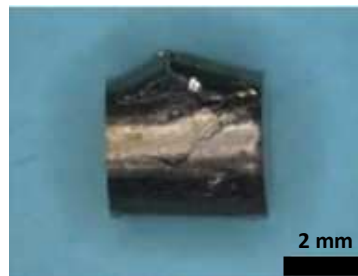
➤ DBTT tested alloys with and without Fe between 600 and 700°C, > 4% Ni increases DBTT

Challenge: Ductile to Brittle Transition Temperature

- DBTT was determined by compression tests at different temperatures



Fracture pattern for $\text{Cr}_{92}\text{Si}_8$
after compression test @
500°C



Fracture pattern for $\text{Cr}_{92}\text{Si}_8$
after compression test @
600°C



Fracture pattern for $\text{Cr}_{92}\text{Si}_8$
after compression test @
700°C

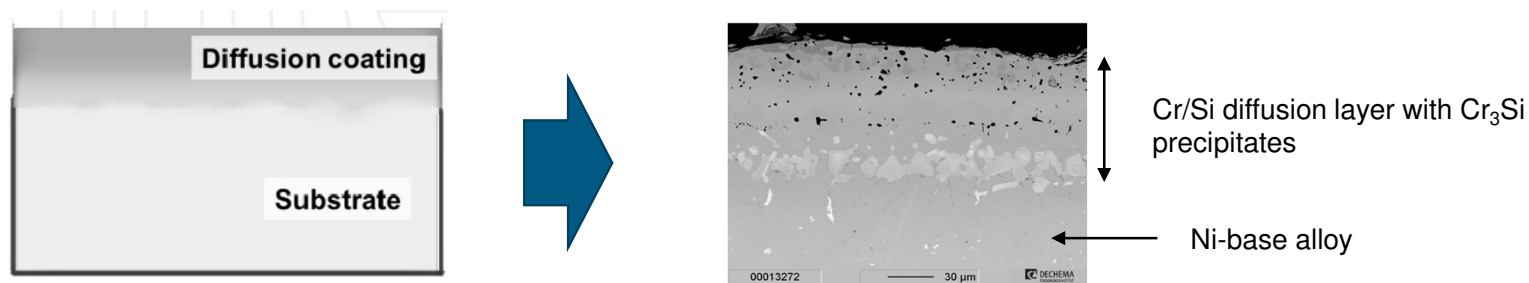
- Up to temperatures to 700°C very limited deformation → DBTT between 600°C and 700°C;
no improvements by alloying with Fe and Ni

Coatings

	Fe	Ni
Fraction of Cr ₃ Si	22 % ↓	41% ↓
Microhardness	28 % ↑	75% ↑
DBTT	→	↑

→ “Make or break” criteria for structural applications →
Development of Cr-Si coatings on state of the art materials as substrates

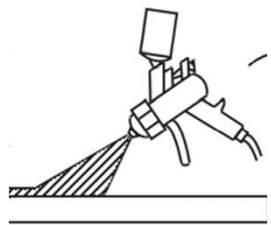
→ Development of Cr/Si diffusion coatings on Fe and Ni-base materials



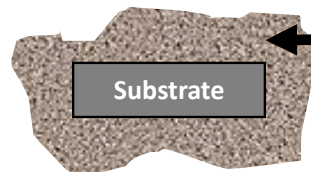
[M.C. Galetz, Coatings for superalloys (2015): 277-296]

Cr-Si Slurry Coating

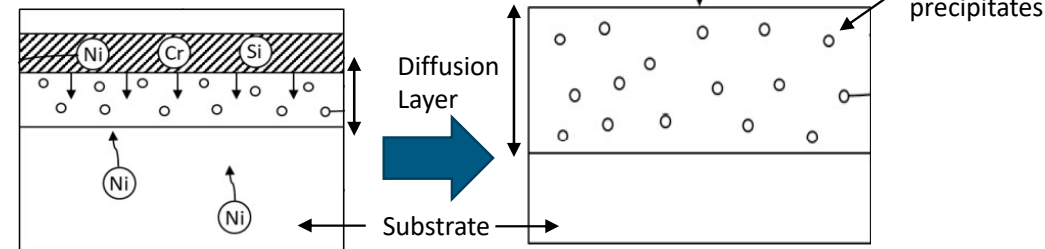
- Newly developed coating process by the slurry technique for applying Cr-Si diffusion coatings



R. Verma et al., Journal of Thermal Spray Technology (2016): 1289-1301



[M.C. Galetz, Coatings for superalloys (2015): 277-296]

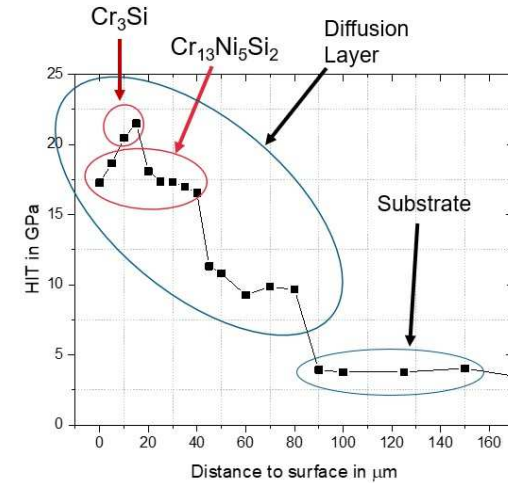
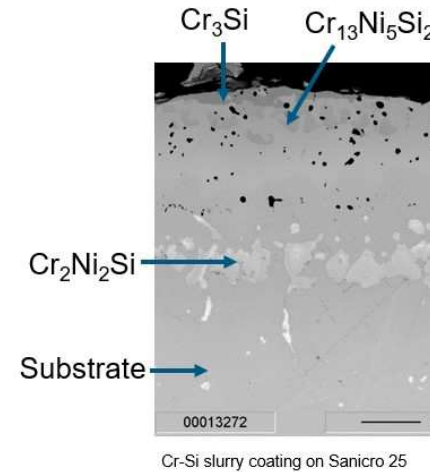


- Enrichment of Cr and Si in surface zone to specifically modify the properties

Cr-Si Coatings: Cross-sections

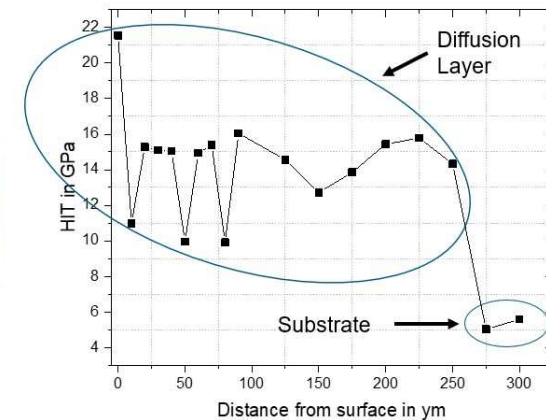
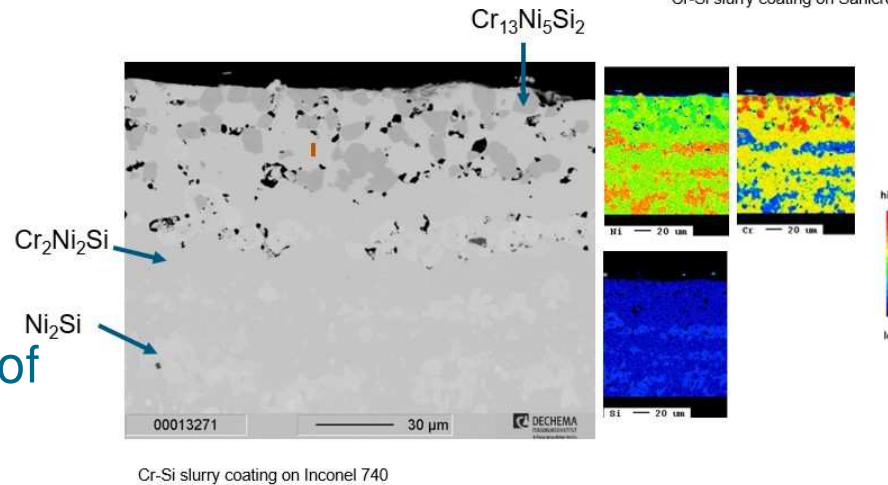
Austenitic steel: Sanicro 25

- Enrichment of Cr and Si in a layer of about 100 μm
- Diffusion layer: high increase of hardness compared to substrate



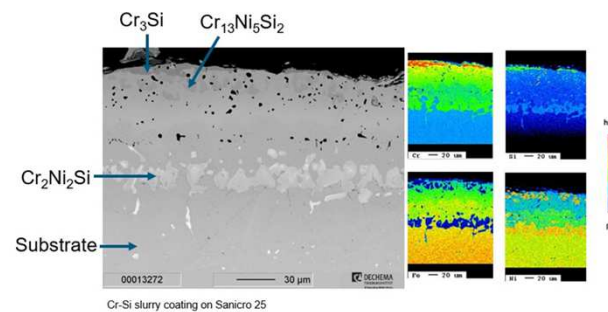
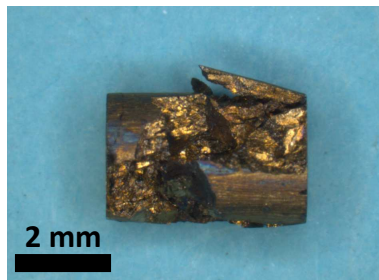
Ni-based alloy: Inconel 740

- Enrichment of Cr and Si in a layer of about 200 μm
- Diffusion layer: high increase of hardness compared to substrate



Conclusions and next steps

- Cr-Si alloys show high potential for high temperature applications
- Mechanical properties and in particular DBTT remains „make or break“ criteria for structural applications



- ***CSP-application: Use Cr-Si in the form of diffusion coatings on state-of-the-art materials: Novel slurry process successfully developed***
- Next Step: Testing of coatings in CSP heat exchanger environment

COMPASSCO2 project website
<https://www.compassco2.eu>

